

METHODOLOGIES FOR TIME DOMAIN FREQUENCY STABILITY MEASUREMENT AND ANALYSIS

W.J. Riley, Hamilton Technical Services

ABSTRACT

This paper describes the most common methodologies for making time domain frequency stability measurements and the ways those data may be analyzed to describe the performance of a frequency source.

INTRODUCTION

The overall steps in performing a frequency stability analysis include data collection, preprocessing, analysis and presentation. This process can be fairly ad hoc for research and development activities, where the results are directed toward discovering, understanding and improving performance, or it can be highly structured for routine production where the expectations are well specified, and the measurement and analysis process may be automated to reduce human workload and to provide consistency. In most cases, the overall process is directed toward extracting performance parameters of the frequency source under test. This paper makes suggestions for implementing such time domain frequency measurements.

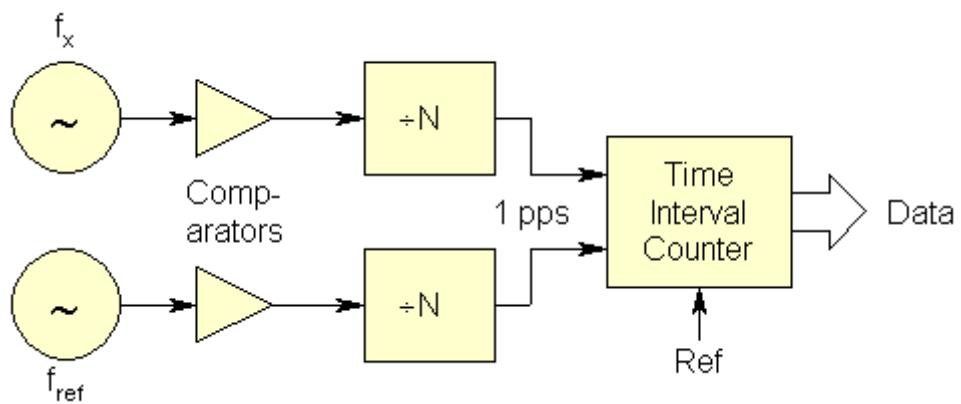
DATA COLLECTION

Stability data must be of the proper type (phase or frequency), sampling interval (τ), resolution, and duration (# samples) to support the analysis required. Phase data is almost always preferable because frequency data can be obtained from it but not vice-versa. There are instances, however, where frequency data is more convenient to gather, observe and analyze. For example, a stability estimate can be made directly from a stripchart record of frequency data, and outliers are more easily identified and removed. The sampling time must be at least as short as the smallest averaging time of interest, and the measurement resolution should be an order-of-magnitude greater than the expected stability. It is often desirable to take data at a shorter measurement interval to allow the largest number of overlapping samples for analysis. The duration of the run should be at least an order-of-magnitude longer than the largest averaging time required, and more data will provide greater confidence in the results. In addition, stability and accuracy of the reference source must be sufficient to support the intended measurement.

Three methods are commonly used for making precise time and frequency measurements, as described below:

- **Time Interval Counter Method**

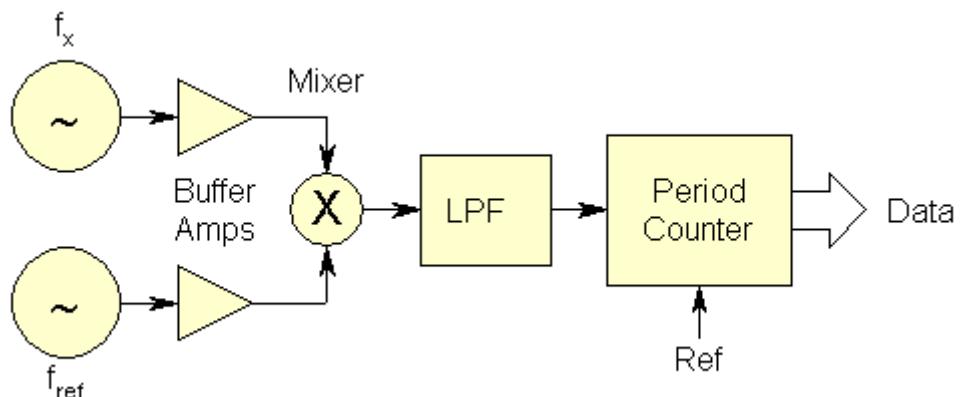
The time interval counter method divides the two sources being compared down to a much lower frequency (typically 1 pps) and measures their time difference with a high resolution time interval counter:



This measurement method is made practical by modern high-resolution interpolating time interval counters that offer 10-digit/second resolution. The resolution is not affected by the division ratio, which sets the minimum measurement time, and, along with the frequency offset, determines how long data can be taken before experiencing a phase spillover (which can be hard to remove from a data set). A source having a frequency offset of 1×10^{-6} can, for example, be measured for only about 5.8 days before experiencing a 1 pps phase spillover after being initially set at the center.

• Heterodyne Method

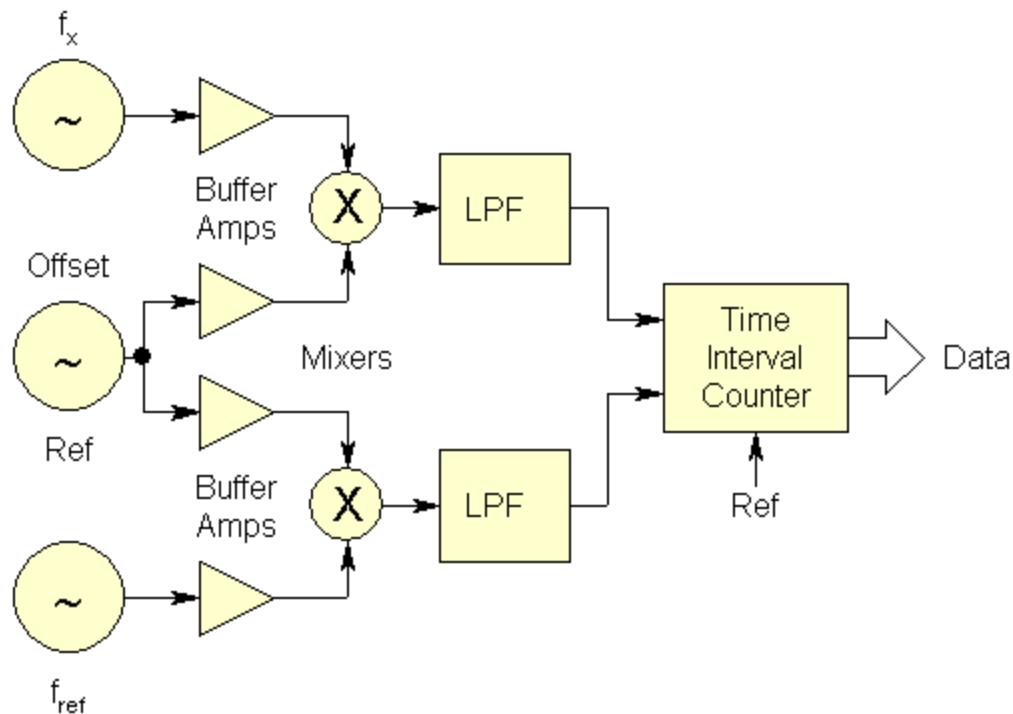
The heterodyne method mixes (subtracts) the two sources being compared, and measures the period of the resulting audio-frequency beat note. The measurement resolution is increased by the heterodyne factor (the ratio of the carrier to the beat frequency).



This heterodyne technique is a classic way to obtain high resolution with an ordinary period counter. It is based on the principle that phase information is preserved in a mixing process. For example, mixing a 10 MHz source against a 9.9999 MHz reference will produce a 100 Hz beat signal whose period variations are enhanced by a factor of $10 \text{ MHz}/100 \text{ Hz} = 10^5$. Thus a period counter with 100 nanosecond resolution (10 MHz clock) can resolve clock phase changes of 1 picosecond. A disadvantage of this approach is that a stable offset reference is required at exactly the right frequency. Even worse, it can only make frequency measurements, requires a priori knowledge of the sense of the frequency difference, and has dead time between measurements.

- Dual Mixer Time Difference

The third method, in effect, combines the best features of the first two, using a time interval counter to measure the relative phase of the beat signals from a pair of mixers driven from a common offset reference:



This dual mixer time difference (DMTD) setup is arguably the most precise way of measuring an ensemble of clocks all having the same nominal frequency. When expanded to multiple channels by adding additional buffer amplifiers and mixers, and time tagging the zero-crossings of the beat notes for each channel, this arrangement allows any two of the clocks to be intercompared. The offset reference need not be coherent, nor must it have particularly low noise or high accuracy, because its effect cancels out in the overall measurement process. For best cancellation, the zero-crossings should be coincident or interpolated to a common epoch. Additional counters can be used to count the whole beatnote cycles to eliminate their ambiguity, or the zero-crossings can simply be time tagged. The measuring system resolution is determined by the time interval counter or timetagging hardware, and the mixer heterodyne factor. For example, if two 5 MHz sources are mixed against a common 5 MHz - 10 Hz offset oscillator (providing a $5 \times 10^6 / 10 = 5 \times 10^5$ heterodyne factor), and the beatnote is timetagged with a resolution of 100 nsec (10 MHz clock), the measuring overall system resolution is $10^{-7} / 5 \times 10^5 = 0.2$ psec.

Multichannel DMTD clock measuring systems have been utilized by leading national and commercial metrology laboratories for a number of years [1-5, 18-20]. An early commercial version is described in Reference [3], a newer technique is described in Reference [8], and the Timing Solutions Corporation TS-3020 is an example of such a system [6]. The Stable32 software [11] has capabilities for reading the data files created by a TS-3020 system, allowing clock records to be conveniently processed.

- Direct RF and IF Signal Digitization

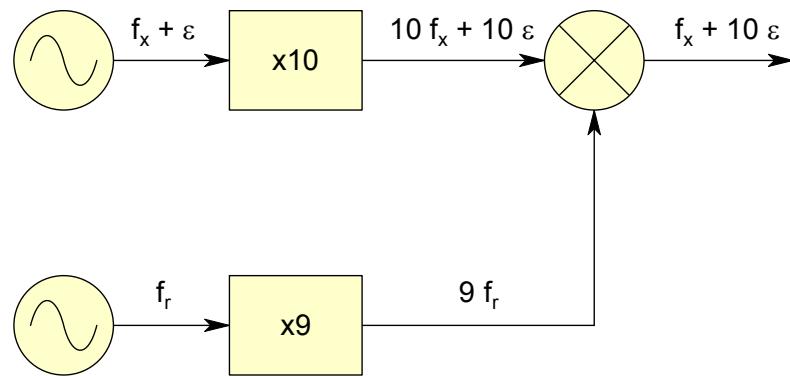
Phase and frequency measurements can be made by using an analog to digital converter (ADC) to digitize either the clock RF signal or the IF signal from a heterodyne measuring system. The Timing Solutions (now Symmetricom) Model TSC 5120A Phase Noise Test Set is an example of the use of direct RF digitization [12] for both time and frequency domain measurements, while JPL [13] and AMSAT [14] have developed special purpose time and frequency domain measurement systems using digitization of the IF signal, the latter employing a PC sound card. Those techniques use digital signal processing (DSP) to estimate the phase of the sampled beat signal.

- Cross Correlation Techniques

Cross correlation using a pair of independent phase measurements can be used to reduce the noise of the measurement system [12]. This technique can be used to reduce the noise floor of both time and frequency domain measurements [15].

- Frequency Error Multiplication

The resolution of frequency measurements can be increased by a process of error multiplication whereby the unknown and reference frequencies are multiplied by factors of N and N-1 respectively and then mixed to obtain the original nominal unknown frequency with its frequency difference increased by a factor N as shown for N=10 in the figure below:



This technique can be applied multiple times to any of the time and frequency domain measurement methods, including the direct use of a frequency counter or RF spectrum analyzer. It is generally limited to a single carrier frequency, and the results depend critically on the noise of the multipliers, the RF filtration, isolation and shielding, and the crosstalk between the signals. Narrowband filtration limits the range of useful sideband frequencies. Resolution enhancements of 10^4 are possible with careful implementation.

- Comparison Between Systems

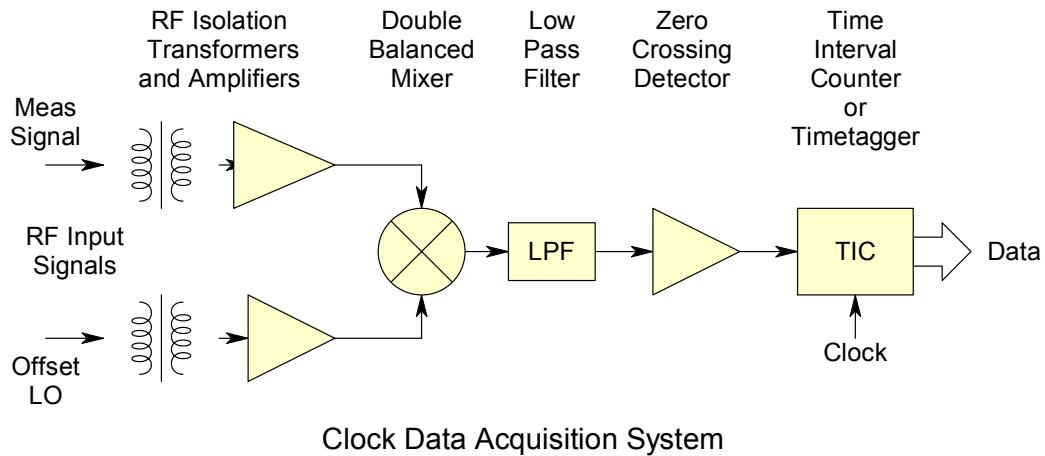
A comparison of the relative advantages and disadvantages of these methods is shown in the following table:

Comparison of Time and Frequency Measurement Methods		
Method	Advantages	Disadvantages
Divider and Time Interval Counter	Provides phase data Covers wide range of carrier frequencies Easily expandable at low cost	Modest resolution Not suitable for short τ
Mixer and Period Counter	Resolution enhanced by heterodyne factor Provides direct frequency data Usable for short τ Expandable at reasonable cost	No phase data No frequency sense Requires offset reference Single carrier frequency
Dual Mixer Time Difference	High resolution, low noise Provides phase data Offset reference noise and inaccuracy cancels No fixed reference channel	Single carrier frequency Relatively complex
RF and IF Signal Digitization	Flexibility, automation	More complex
Crosscorrelation	Lower noise floor	More complex
Error Multiplication	Higher resolution	Narrowband

Other examples of commercial instruments capable of producing 1-second numeric data with exceptionally low noise and high resolution are the Timing Solutions Corporation Model 5110A Time Interval Analyzer [6] and the Quartzlock Model A7 Frequency & Phase Comparator [7]. Both of those instruments have been used with the Stable32 program to perform state-of-the-art frequency stability measurements.

• Data Acquisition

A typical data acquisition system for clock measurements is shown in the figure below. This can represent either a heterodyne measurement system, or one channel of a dual mixer time difference measurement (DMTD) system.



The RF signals are isolated by RF transformers to avoid ground loops, and by isolation amplifiers to provide good input cable termination and reverse isolation for mixer products. It is important that those components have low phase sensitivity to temperature variations. The mixer is followed by a low pass filter to separate the audio beat signal from the RF components. The most critical component is the zero crossing detector or comparator that converts the analog beat signal into a digital waveform. It must have

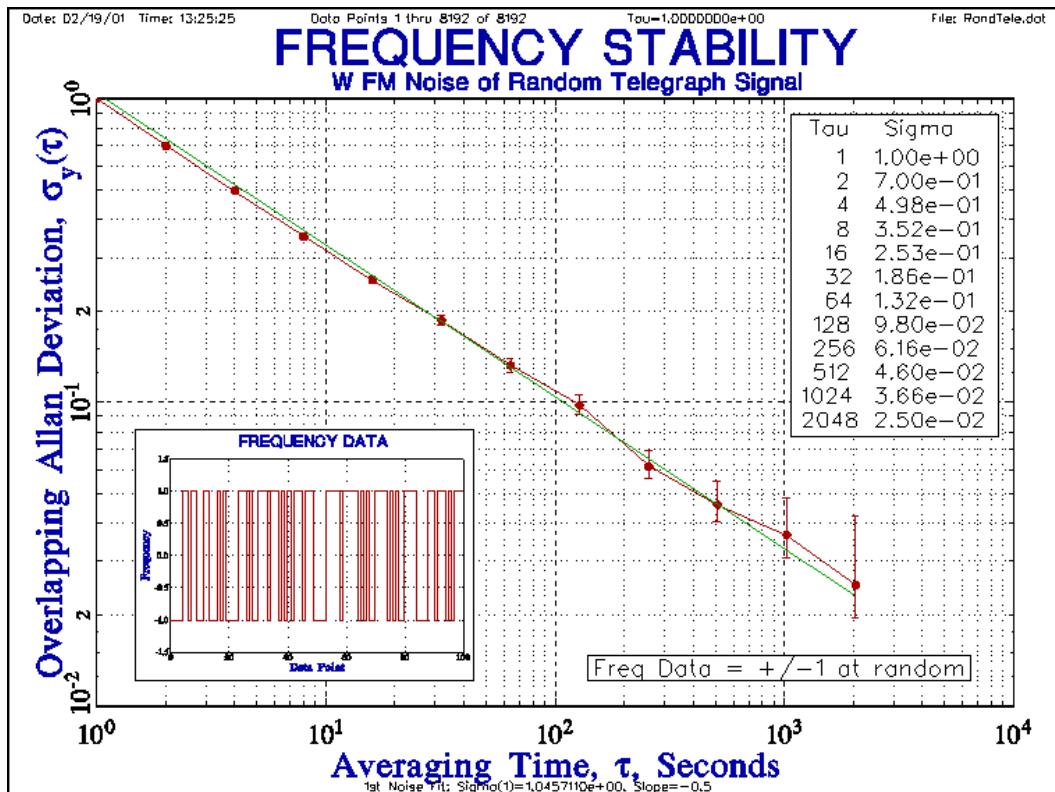
low noise and offset, and high speed so that the relatively slow beat signal is converted to a fast switching signal with low jitter at its exact zero crossing, and without crosstalk between adjacent channels [16].

The zero crossing detector output becomes one input of a time interval counter, or is timetagged by a digitizer with respect to an external system clock. The former is most commonly used for a simple heterodyne system, while the latter is generally used in a multi-channel DMTD system. Because of the large heterodyne factor that is normally used (e.g., 10^6 for a 10 Hz beat note with 10 MHz signals), high measurement resolution does not require particularly fast time measurements (e.g., 0.1 psec overall resolution for a 10 MHz clock).

It is important to understand the potential vulnerability of a clock data acquisition system to interfering signals such as power line ripple. Signals at frequencies higher than one-half the sampling rate (e.g. 5 Hz for a 10 Hz beat note) are aliased and appear in the data as interference at lower frequencies. The system does not, and, as a practical matter, cannot have, low pass filtration to avoid such aliasing. Hence the importance of the RF isolation transformers and other precautions to avoid contamination by interfering signals. One should be alert to strange results, such as oscillations in an Allan deviation plot, which can be a sign of an aliasing problem. A higher beat frequency and sampling rate, perhaps followed by digital low pass filtration and decimation, is another way to reduce those problems, at the expense of lower resolution or the need for a higher performance time digitizer. Satisfactory results are usually obtained, as long as one remains aware of the possibility of aliasing difficulties.

• Phase Data Quantization

While it is desirable to have sufficient resolution so that the data is noise rather than resolution limited, highly quantized data can provide good stability information provided that there is a least 1 bit of meaningful variation, as shown in the following plot for a random telegraph signal representing frequency data having a white FM noise characteristic:



DATA PREPROCESSING

- **Outlier Detection**

It is not unusual for frequency stability data to contain outliers, especially for large data sets that extend over long measurement runs. Such outliers must be identified, explained, and removed in order to use the rest of the data. The Stable32 program includes robust outlier detection based on median statistics.

- **Plotting**

Data plotting is an important technique not only for formal analysis, but also as a preprocessing step to become familiar with the data and to plan its analysis. Never underestimate the insight that effective data visualization can provide. An example of the importance of data plotting is a recognition that the results of a measurement are contaminated by some form of environmental sensitivity (see All Tau Analysis below).

- **Drift Removal**

Frequency drift is present in most frequency sources, and its modeling and removal is an important step both for its own sake in characterizing the drift, and to separate the deterministic drift from the stochastic noise for further analysis. The Stable32 program supports a number of drift models for phase and frequency data.

- **Problems and Pitfalls**

It can be difficult to distinguish between a bad unit under test and a bad measurement. When problems occur in time-domain frequency stability measurements, they almost always cause results that are worse than expected. It is nearly impossible for a measurement problem to give better than correct results, and there is considerable justification in saying that the best results are the correct ones. Two possible exceptions to this are (1) misinterpretation of the scale factor, and (2) inadvertent coherency (e.g. injection locking of one source to another due to inadequate isolation). Lack of stationarity (changes in the source itself), while not a measurement problem per se, must also be considered (a dynamic stability analysis [17], available in Stable32, can be used to detect such behavioral changes). In general, the more devices available and the more measurements being made, the easier it is to sort things out.

One common problem is hum that contaminates the measurements due to ground loops. Because the measurement interval is usually much longer than the period of the power line frequency, and not necessarily coherent with it, aliased "beats" occur in the frequency record. Inspection of the raw data can show this, and the best cure is often isolation transformers in the signal leads. In fact, this is a wise precaution to take in all cases.

All sorts of other mechanisms exist that can interfere with time domain frequency measurements (electrical, electromagnetic, magnetic, thermal, barometric, vibrational, acoustic, etc.). Consider all the environmental sensitivities of the unit under test, and control as many of them as possible. Be alert to day-night and weekly cycles that indicate human interference. Stories abound about correlations between elevators moving and cars coming and going ("auto-correlations") that have affected clock measurements. Think about what can change in the overall test setup. Slow periodic fluctuations will show up more distinctly in an all tau (rather than an octave tau) stability plot.

In high-precision measurements, where picoseconds matter (e.g. $1 \times 10^{-15} = 1 \text{ psec}/1000 \text{ seconds}$), it is important to consider the mechanical rigidity of the test setup (e.g. $1 \text{ psec} = 0.3 \text{ mm}$). This includes the

electrical length (phase stability) of the connecting cables. Teflon dielectric is an especially bad choice for temperature stability, while foamed polyethylene is much better. Even a few degrees of temperature variation will cause the phase of a high-stability source to "breathe" as it passes through 100 feet of coaxial cable.

Phase jumps are a problem that should never be ignored. Examination of the raw phase record is critical because a phase jump (frequency impulse) appears strangely in a frequency record as a white FM noise characteristic [10]. Some large phase jumps are related to the carrier period, which can be caused by a malfunctioning frequency divider.

DATA ANALYSIS

- **Stability Analysis**

The most common frequency stability measure is the overlapping Allan (2-sample) deviation, $\sigma_y(\tau)$. That statistic is used to express time domain frequency stability in most cases, and should be used in preference to the classic non-overlapped or "normal" Allan deviation unless there is some particular reason for doing otherwise. The overlapping Allan deviation has the same expected value while providing better confidence. If the frequency source has significant drift, then it is usually removed before performing the stability analysis so that the deterministic and stochastic aspects of the frequency stability can be expressed separately. An alternative is to use the Hadamard (3-sample) deviation which produces the same result as the Allan deviation in the presence of linear frequency drift. Again, the overlapping Hadamard deviation is usually a better choice than its non-overlapping equivalent. If the frequency source is known or suspected to have a highly-divergent (flicker walk or random run FM) noise characteristic, then a Hadamard deviation should definitely be used to provide a meaningful result.

If stability information at the longest possible averaging time is important, then the total versions of the 2-sample (TOTDEV) or 3-sample (HTOT) deviations, or the newer Théorstatistic (which can provide useful stability information at 75% of the record length) should be considered. Those statistics, available in Stable32, offer better confidence at large averaging factors at the expense of longer computation time.

If the data being analyzed exhibits a white or flicker PM noise characteristic, then the modified Allan (MDEV) or modified total MTOT) deviation can be used to resolve the ambiguity between those noise types.

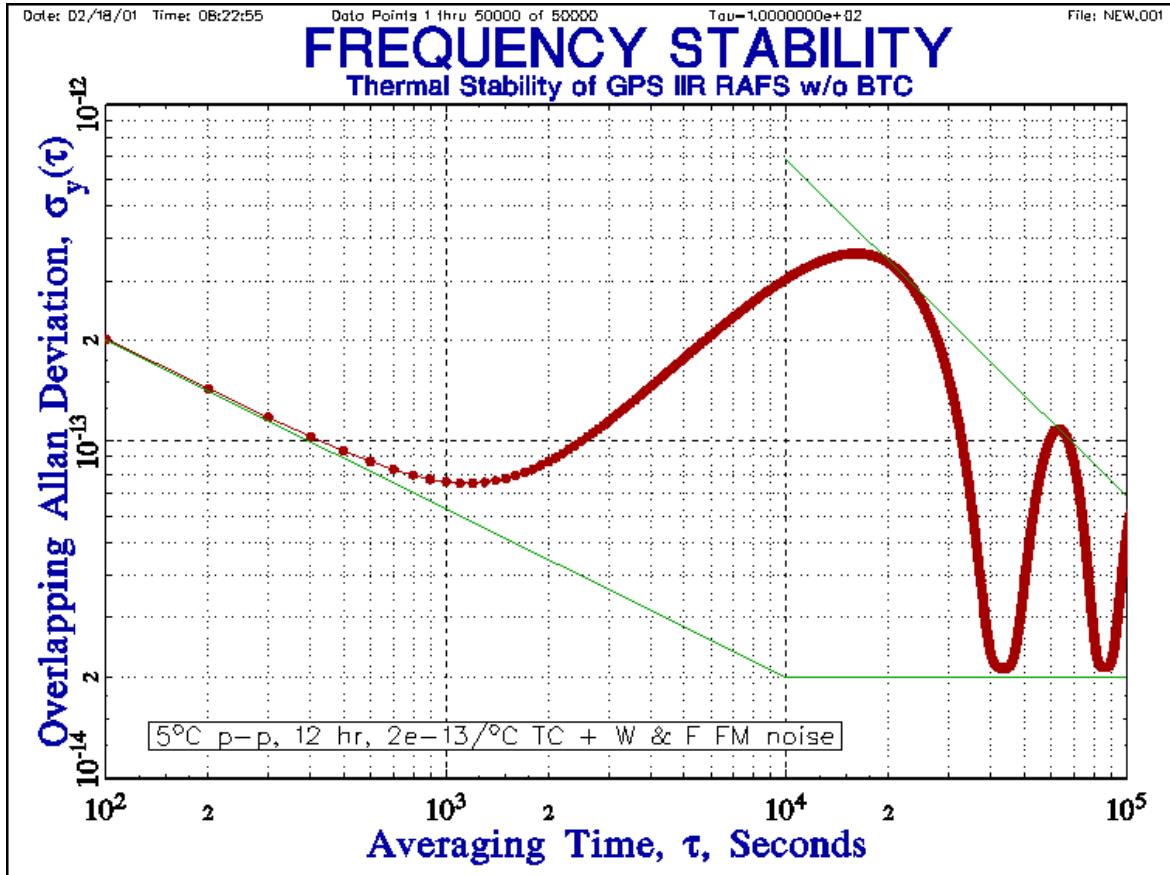
- **All Tau Analysis**

Performing a stability analysis at all possible averaging times (τ) is a form of spectral analysis that can provide important insight into the stability of a frequency source, particularly when the device is subject to some periodic influence such as temperature cycling. The combination of an environmental sensitivity and a cyclic disturbance will cause the time-domain stability to display a distinctive pattern of maxima and minima at the half period and period of the stimulus as given by the expression:

$$\sigma_y(\tau) = \frac{\Delta f/f}{\pi} \cdot \frac{T}{\tau} \sin^2\left(\pi \cdot \frac{\tau}{T}\right)$$

where: $\Delta f/f$ = peak frequency deviation, T = period of disturbance, and τ = averaging time.

An example of such a stability record is shown below. This is a simulation of the stability of a GPS Block IIR rubidium atomic frequency standard (RAFS) with typical white and flicker noise levels of $2 \times 10^{-12} \tau^{-1/2}$ and 2×10^{-14} respectively, plus a temperature coefficient of $2 \times 10^{-13}/^\circ\text{C}$, when exposed to a sinusoidal orbital temperature variation of 5°C p-p with a 12-hour period. The actual clock has a baseplate temperature controller (BTC) that reduces this thermal sensitivity to below the noise level. Even this large periodic variation does not prevent determining the underlying noise level.



This stability plot clearly shows the effect of the periodic disturbance. The worst case occurs at one-half the orbital period (6 hours) where, without the BTC, the RAFS stability is degraded by a factor of ten to 3.2×10^{-13} , compared with a normal stability of about 3.4×10^{-14} at that averaging time.

A stability analysis at every possible tau produce a plot with this shape indicate that a periodic effect is disturbing the frequency. In the frequency domain, the Allan variance has a broad peak at Fourier frequency $f=1/2\tau$ with a bandwidth $BW=1/2\pi\tau$.

DATA PRESENTATION

The results of a stability analysis are usually presented as a combination of textual, tabular and graphic forms. The text describes the device under test, the test setup, and the methodology of the data preprocessing and analysis, and summarizes the results. The latter often includes a table of the stability statistics. Graphical presentation of the data at each stage of the analysis is generally the most important aspect of presenting the results. For example, these are often a series of plots showing the phase and frequency data with an aging fit, phase and frequency residuals with the aging removed, and stability plots with noise fits and error bars. Plot titles, sub-titles, annotations and inserts can be used to clarify and

emphasize the data presentation. The results of several stability runs can be combined, possibly along with specification limits, into a single composite plot. The various elements can be combined into a single electronic document for easy printing and transmittal.

VALIDATION

It is important to validate all aspects of the measurement and analysis process. This includes verifying the resolution, scale factor, sense, noise floor, and environmental sensitivity.

Validation of the measurement hardware can be done by (1) making coherent measurements, (2) checking multiple sources and references, (3) comparison against other measurement equipment, and (4) making known phase and frequency changes. The latter can be done by changing cable length, adjusting synthesizer settings, or oscillator tuning voltages.

Validation of the analysis tools is made easier by using commercially-available products. Other validation methods include (1) manual analysis of small data sets, (2) comparison against published results, (3) comparison against other stability analysis programs, (4) comparison against general purpose mathematical and spreadsheet programs, (5) consistency checks for different data types, variances and analysis methods, and (6) checks against simulated clock data.

AUTOMATION

Frequency measurement and analysis systems can benefit significantly from automation. Making their operation automatic provides consistency, reduces errors, and allows routine processes to be done by lower-skilled personnel. For the measurement hardware, this involves computer control. For the analysis, this may involve writing batch scripts. The Stable32 program includes a built-in scripting capability for automating a frequency stability analysis.

REFERENCES

1. D.W. Allan, "[Picosecond Time Difference Measurement System](#)", *Proc. 29th Annu. Symp. on Freq. Contrl.*, pp. 404-411, May 1975.
2. D.A. Howe, D.W. Allan and J.A. Barnes, "[Properties of Signal Sources and Measurement Methods](#)", *Proc. 35th Annu. Symp. on Freq. Contrl.*, May 1981, pp. 1-47.
3. S.R. Stein, "[Frequency and Time - Their Measurement and Characterization](#)", Chapter 12, pp.191-416, *Precision Frequency Control*, Vol. 2, Edited by E.A. Gerber and A. Ballato, Academic Press, New York, 1985, ISBN 0-12-280602-6.
4. S. Stein, D. Glaze, J. Levine, J. Gray, D. Hilliard, D. Howe and L. Erb, "[Performance of an Automated High Accuracy Phase Measurement System](#)", *Proc. 36th Annu. Freq. Contrl. Symp.*, June 1982, pp. 314-320.
5. S.R. Stein and G.A. Gifford, "[Software for Two Automated Time Measurement Systems](#)", *Proc. 38th Annu. Freq. Contrl. Symp.*, June 1984, pp. 483-486.
6. Data Sheet, [Model 5110 Time Interval Analyzer](#), [Timing Solutions Corporation](#) 5335 Sterling Dr, Suite B Boulder, CO 80301 USA.
7. Data Sheet, [A7 Frequency & Phase Comparator Measurement System](#), [Quartzlock \(UK\) Ltd.](#), Gothic, Plymouth Road, Totnes, Devon, TQ9 5LH England.
8. C.A. Greenhall, "[Oscillator-Stability Analyzer Based on a Time-Tag Counter](#)", *NASA Tech Briefs*, NPO-20749, May 2001, p. 48.

9. Gernot M.R. Winkler, "[Introduction to Robust Statistics and Data Filtering](#)", Tutorial at 1993 IEEE Freq. Contrl. Symp., Sessions 3D and 4D, June 1, 1993.
10. C.A. Greenhall, "[Frequency Stability Review](#)", Telecommunications and Data Acquisition Progress Report 42-88, Oct-Dec 1986, Jet Propulsion Laboratory, Pasadena, CA, pp. 200-212, Feb. 1987.
11. Data Sheet, [Stable32 Software Package for Frequency Stability Analysis](#), Hamilton Technical Services, Beaufort, SC 29907 USA.
12. *Operations and Maintenance Manual*, TSC 5120A Phase Noise Test Set, Timing Solutions Corporation, Boulder, CO 80301, Rev. G, May 16, 2006.
13. C.A. Greenhall, "Digital Signal Processing in the Radio Science Stability Analyzer", TDA Progress Report 42-121, Jet Propulsion Laboratory, Pasadena, California, May 15, 1995.
14. See <http://www.go-mars.org>.
15. 1. W.F. Walls, "[Cross-Correlation Phase Noise Measurements](#)", *Proceedings of the 1992 IEEE Frequency Control Symposium*, pp. 257-261, May 1992.
16. 1. G.J. Dick, P.F. Kuhnle, and R.L. Sydnor, "Zero Crossing Detector with Sub-Microsecond Jitter and Crosstalk", *Proceedings of the 22nd Precise Time and Time Interval (PTTI) Applications and Planning Meeting*, December 1990, pp. 269-282.
17. L. Galleani and P. Tavella, "[Tracking Nonstationarities in Clock Noises Using the Dynamic Allan Variance](#)", *Proc. 2005 Joint FCS/PTTI Meeting*, August 2005, pp. 392-396.
18. L. Sojdr, J. Cermak, and R. Barillet, "[Optimization of Dual-Mixer Time-Difference Multiplier](#)", Institute of Radio Engineering and Electronics, Czech Academy of Sciences, Czech Republic, and Observatoire de Paris, Paris, France.
19. L. Sojdr, J. Cermak, and G. Brida, "[Comparison of High-Precision Frequency Stability Measurement Systems](#)", *Proceedings of the Joint 2003 IEEE Frequency Control Symposium/17th EFTF Meeting*, May 2003, pp. 317-325.
20. C.A. Greenhall, A. Kirk, and R.L. Tjoelker, "[A Multi-Channel Stability Analyzer for frequency Standards in the Deep Space Network](#)", *Proceedings of the 38th Precise Time and Time Interval (PTTI) Applications and Planning Meeting*, December 2006, pp. 105-115.

File: METHODOLOGIES.doc
 W.J. Riley
 Hamilton Technical Services
 September 12, 2007